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ABSTRACT

Method and apparatus for delivering aerosolized medication employing a variable volume device and a chamber reservoir.

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Invention Title:
"METHOD AND APPARATUS FOR DELIVERING AEROSOLIZED MEDICATION".

Details of Associated Provisional Application No(s):

The following abstract is a full description of this invention including the best method of performing it known to us.

METHOD AND APPARATUS FOR DELIVERING

AEROSOLIZED MEDICATION

Field of the Invention

The present application, which is a divisional application derived from Application No. 1004/99, relates to methods and apparatus for delivering a dose of aerosolized medication for inhalation by a patient into the lungs.

Background of the Invention

Apparatus are increasingly being used for delivering medication for therapeutic treatment of the lungs. For example, in the treatment of asthma, inhalers are commonly used for delivering bronchodilators such as β_2 agonists and anti-inflammatory agents such as corticosteroids. Two types of inhalers are in common use, pressurised dose inhalers (PMDIs) and dry powder inhalers (DPIs). Both types have as their object the delivery of medication, which is typically in the form of a solid particulate or powder, into the airways of the lungs or the lumen of the trachea being treated.

In the MDI device, the medication is provided by the pharmaceutical manufacturer in a pressurised metal container, with the medication being released

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or dispersed in a liquid propellant such as a chloroform-sulfur (CFC) or hydrocarbon-sulfur (DFA). The container includes a venting valve having a bellows discharge such which can be depressed inward into the container to discharge a controlled volume of propellant-oxidant mixture in the form of an aerosol comprising the droplets of propellant in which particles of the medication are suspended or dissolved. A typical MDI for use with such a container includes a housing having an actuator and nozzle. The container is housed into the housing with the bellows discharge means of the container being received in a hole in the actuator. Depressing the closed end of the container causes the aerosol to be pushed inward into the container so that a controlled volume of medication is discharged through the nozzle. The housing further defines a throat in fluid communication with the nozzle, the throat having an outlet as a multiphase jet of the aerosol, such that the aerosolized medication may be inhaled after it exits the multiphase jet. The patient either breathes the medication into the throat with the lips closed around the nozzle, or inhales the medication in a slight vacuum away from an open mouth. The patient then depresses the container to discharge the medication, and subsequently inhales.

Existing MDIs suffer from a number of significant shortcomings. One problem with existing MDIs is poor delivery efficiency of the medication. It has been estimated that on average, with existing MDIs, only about 10 percent of the

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medication dose which is discharged from the container actually reaches the lungs where it can achieve the intended effect.

Poor delivery efficiency is caused by a number of factors. One of these is incomplete evaporation of propellant, resulting in a large portion of the aerosol dose being delivered in a form which cannot be inhaled into the lungs. For effective delivery of aerosolized medication to the droplets of the lungs, it is desirable that most of the particles which are inhaled be less than about 10 microns (one micron=one-thousandth of a millimeter) in size, and preferably between about 1 micron and 5 microns. Incomplete evaporation of propellant in the mouth of the multiphase nozzle is a substantial fraction of the aerosol dose being delivered in the form of relatively large liquid droplets instead of fine dry particles whose vapor. Such droplets cannot be inhaled, but rather tend to impact the inside of the mouth and at the back of the patient's throat, with the result that much of the medication is swallowed. The local concentration of medication in the mouth and throat can cause local immune-suppression responses, as well as development of fungal infections in the case of corticosteroids. Additionally, swallowing it, reduces some effectiveness of the aerosolized medication of the pharmaceutical agent, which decreases consistency and activity of the treatment. Further, the wasted medication has been estimated to cost U.S. patients about \$750 million per year.

Another factor contributing to the problem of poor delivery efficiency is high linear velocity of the aerosol as it exits the multiphase nozzle, which tends to lead to

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impaction of the aerosol in the mouth and throat. Ideally, the velocity of the aerosol should match the velocity of the patient's inspired breath so that the particles are absorbed in the lungs and do not exit into the lungs. With many existing MDIs, the exit velocity of the aerosol substantially exceeds the velocity of the patient's breath. The high-velocity plume strikes the back of the throat, causing impaction and choking. The mouth further contributes to the poor delivery efficiency of existing MDIs in excessive length of the plume or hole of aerosol exiting the device. In existing MDIs, this length typically exceeds 20 centimeters, which causes it to choke the patient as he inhales the aerosol.

In an effort to decrease plume velocity, some MDI designs have added internal baffles between the aerosol nozzle and the multiphase nozzle. Although baffles improve delivery efficiency, none of the drug which is discharged from the nozzle impacts and acts on the inner surfaces of the plume, and is therefore unavailable for inhalation by the user. Thus, MDIs with baffles still suffer from inadequately low delivery efficiency.

Furthermore, although dry powder inhalers inherently avoid some of the shortcomings of MDIs, such as excessive aerosol velocity, DPHs still suffer from the problems of impaction and choking of medication in the inner surfaces of the device, particularly under certain circumstances such as high relative humidity, which tends to cause particle agglomeration.

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Another problem with existing MDIs is the difficulty patients have in coordinating their inhalation with the discharge of the aerosol. In normally operated MDIs, patients frequently inhale too early or too late or effectively ignore the medication. Although a number of breath-actuated MDIs have been devised to address this problem, none of these devices senses discharge at the very onset of the patient's inspiratory effort. Depending on the time condition being sensed and its location, it may either be more desirable for the medication to be discharged near the peak of the patient's inhalation rather than the beginning. Further, it may be desirable to be able to selectively vary the point in the patient's inhalation at which medication is discharged in order to alter the location of drug delivery in the respiratory tract. These advantages are not possible with existing MDIs.

Accordingly, it has been an object of the present invention to provide a method and apparatus for delivering an aerosolized medication in which the magnitude of the aerosol dose (i.e., the fraction of the dose of dry particles of the medication which is inhaled) is controlled in the rate of the apparatus.

It has been a further object of the present invention to provide a method and apparatus for delivering an aerosolized medication in which the linear velocity of the aerosol in the rate of the apparatus approximately matches the velocity of the patient's inspired breath.

It has been another object of the invention to minimize degradation and clogging of the drug particles in the hole of an aerosol nozzle or similar apparatus.

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It has been a well known object of the present invention to provide a method and apparatus for delivering an aerosolized medication to which the lungs of the body of a patient are subjected.

A further object of the invention has been to provide a method and

- 5 apparatus for controlling the respiration of a patient in a hospital.

Still another object of the invention has been to provide a method and apparatus for delivering an aerosolized medication to which a patient and a child of a patient are subjected.

It has been another object of the present invention to provide a method

- 10 and apparatus for delivering an aerosolized medication to which the discharge of a gas is synchronized with the patient's inspired breath, and in which the timing of the discharge is related to the patient's breath can be selectively varied.

Summary of the Invention

The above and other objects of the invention are achieved by the

- 15 method and apparatus of the invention in which flow control techniques and devices are used to produce delivery of the propellant-gas mixture with air to increase respiration of propellant, to draw down the aerosol phase before it reaches the exit of the apparatus, and to reduce the frequency of aerosol on the lower walls of the apparatus. The invention also provides an apparatus and method for synchronizing
- 20 the admission of the patient with the patient's inspiratory effort caused by the movement of the apparatus.

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In one embodiment of the invention, the apparatus is configured so that the mouth discharge orifice directs a phase toward the open end of the mouthpiece.

The air tube is arranged to draw air from the open end of the mouthpiece so as to impinge on the phase.

- 5 The air tube is arranged to draw air from the open end of the mouthpiece so as to impinge on the phase. The air tube is arranged to draw air from the open end of the mouthpiece so as to impinge on the phase. The air tube is arranged to draw air from the open end of the mouthpiece so as to impinge on the phase. The air tube is arranged to draw air from the open end of the mouthpiece so as to impinge on the phase.

- 10 The phase and air jet are drawn, causing mixing and distribution of the phase.
- 15 The mouthpiece of the invention, the mouth is positioned to direct a phase away from the open end of the mouthpiece toward the end of the mouth, which end is substantially closed by an end wall. The air tube is connected to the end wall, with the tube of the air tube connected to a passage through the end wall to achieve air outside the mouth. Substantially by a patient on the open end of the air tube, the air tube is connected to a passage through the end wall to achieve air outside the mouth. Substantially by a patient on the open end of the air tube, the air tube is connected to a passage through the end wall to achieve air outside the mouth.
- 20 The phase and air jet are drawn, causing mixing and distribution of the phase. The phase and air jet are drawn, causing mixing and distribution of the phase. The phase and air jet are drawn, causing mixing and distribution of the phase.

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More specifically, the invention provides a method and apparatus including a housing adapted to support a pressurized container, the housing having an entrance and mouth assembly with a tube adapted to receive the patient's mouth.

- 3 The housing has an open end facing a mouthpiece adapted to be inserted into the mouth of a patient, a mouth discharge orifice of the entrance and mouth assembly being positioned to direct a phase of aerosolized medication into the mouth; and an air tube arranged within the mouth and having an air tube outlet arranged opposite the mouth

discharge orifice and an air tube inlet in fluid communication with ambient air outside the mouth. The air tube being arranged so that air flowing out of the air tube outlet is directed so as to impinge on a phase of aerosolized medication discharged from the

mouth through the mouth discharge orifice. Thus, an inspiratory effort caused by the mouthpiece causes air to flow from the air tube inlet and out the air tube outlet so

impinge on the phase and thereby enhance dispersion and mixing of the medication within the mouth. The air jet from the air tube also causes the phase to draw down so that the velocity of the aerosol exiting the device approximately matches the

velocity of a patient's inspired breath. Drawing down the phase also increases the residence time of the aerosol within the apparatus and leads to a slower release to be inhaled. The increased mixing and residence time produces more complete

- 10 respiration of propellant in the end of the mouthpiece.

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mixing the medication, so that the more length of mouth is used when, thereby further increasing residence time of the aerosol within the device.

To reduce impedance and mixing of medication on the lower walls of the apparatus, the invention provides an aerosol flow control apparatus, useful for

- 5 other MDI or DPI devices, including a housing defining a mouth, the mouth having an open end defining a mouthpiece and a substantially closed end defined by an end wall remote from the mouthpiece, with a medication dispenser assembly being arranged within the housing to direct medication into the mouth. The medication dispenser may be a pressurized container with entrance and mouth, or alternatively may

be a dispenser for medication in dry powder form. The end wall includes a plurality of secondary air tubes in fluid communication with ambient air outside the mouth, the

secondary air tubes opening into the mouth adjacent the lower wall of the mouth, in a direction generally toward the open end of the mouthpiece. The mouth further

includes a plurality of various passages formed on the lower wall thereof

discharge of the secondary air tubes, the secondary air tubes and various passages responding to conditions a reduced air flow along the lower wall of the mouth upon an inspiratory effort being exerted on the mouthpiece. The secondary air flow acts as a buffer or boundary layer flow along the lower wall of the mouth, reducing the

- 10 thickness of aerosol deposits or any particles impinging and prematurely mixing on the lower wall. The various passages preferably comprise laterally directed means

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which are mounted in no angle to the said chamber so as to impart said velocity to the air flowing over them.

The invention further provides an upward flow control apparatus for use with a pressurized chamber of construction, in which discharge of the upward phase is caused by the patient's inspiratory effort, with the timing of the discharge in relation to the inhalation being selectively variable. To these ends, the apparatus includes a housing adapted to support the chamber between a first position in which the discharge area of the chamber is in an inspiratory position in a second position in which the discharge area is in an expiratory position for discharging a measured volume of exhalation, the housing further including an outlet through which a user can inhale, the outlet defining a primary air passage. A chamber restrictor is arranged in the housing and is movable from a first position in which relative movement between the restrictor body and discharge area is prevented to a discharge position in which such movement is permitted. The chamber restrictor forms a part of, or alternatively is, mounted on, a device such as a bellows or a variable displacement pump assembly which defines a variable-volume chamber. The limiter includes a resilient member which urges the chamber into the second position upon compression of the chamber restrictor into its discharge position. A secondary air passage extends through the housing between the primary air passage and restrictor air intake the housing, the secondary air passage including a valve. The variable-volume chamber is in fluid communication with a source of the vacuum, whereby inhalation of a user through the

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FIG. 1 is a perspective view of an inhaler in accordance with the principles of the present invention.

FIG. 2 is an exploded view of the inhaler of FIG. 1.

FIG. 3 is a cross-sectional view of the inhaler taken along lines 3-3 of

FIG. 1.

FIG. 3A is a partial cross-sectional view showing an alternative construction of the chamber and outlet of the inhaler.

FIG. 4 is a cross-sectional view similar to FIG. 3, showing an alternative construction of the inhaler.

FIG. 5 is a cross-sectional view similar to FIG. 3, showing yet another alternative construction of the inhaler.

FIG. 6 is a cross-sectional view of the inhaler of FIG. 3 taken on a plane normal to that of FIG. 3.

FIG. 7 is a cross-sectional view of a chamber alternative construction of the invention, having features for achieving separate suction of a chamber responsive to a patient's inhalation through the inhaler.

FIG. 8 is a perspective view of the trigger which engages and disengages the restrictor in the inhaler of FIG. 7.

FIG. 9 is side elevational view, partly in cross-section, of yet another alternative of the invention, showing an alternative arrangement for achieving separate suction of a chamber responsive to a patient's breath.

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which causes a low pressure in the upward down so as to increase air flow. The restrictor and thereby cause the chamber restrictor to move into the discharge position. By appropriate selection of design parameters such as the chamber cross-sectional area, the flow created by the restrictor member on the chamber, the vacuum size, and the secondary air passage diameter, the device can be designed to cause suction of the chamber near the point of a patient's inspiratory effort.

The device preferably further includes means for selectively varying the timing of suction. For instance, the device may include an adjustment screw for varying the secondary air passage to act as a variable flow restrictor. Turning the screw one direction increases the amount of flow restriction, such that the flow impedance rate through the restrictor, the amount of flow required to overcome the chamber sufficiently to cause suction is increased. Conversely, turning the screw in the opposite direction decreases the amount of flow required to cause suction.

There are other objects and advantages of the present invention that become more apparent from the accompanying drawings and the description thereof. Brief Description of the Drawings

The accompanying drawings, which are incorporated in and constitute a part of this specification, illustrate various embodiments of the invention and, together with the general description of the invention given above and the detailed description given below, serve to explain the principles of the invention.

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Brief Description of the Drawings

FIGS. 1-3 depict a first embodiment of an inhaler in accordance with the principles of the invention. The inhaler 10 includes a housing 12 which has a respiratory portion 14 connected to a mouth 16. The respiratory portion 14 is in the form of a device adapted to receive a standard pressurized container 18 containing a medication. The container 18 forms one part of the present invention. The inhaler operates on the principle of the present invention in which any standard pressurized container having an internal venting valve with a hollow discharge area which may be depressed laterally with respect to the restrictor body from an inspiratory position in which discharge of medication is prevented, to an expiratory position in which a measured volume of the chamber restrictor is discharged through the hollow discharge area.

The restrictor 16 includes an open end 20 spaced from the respiratory portion 14, and a closed end 22 defined by an end wall 24 which is connected to the respiratory portion 14. The end wall 24 preferably is generally rounded on its outer surface, with an apex of the end wall 24 defining the portion of the end wall 24 furthest from the open end 20.

With reference to FIG. 3, the housing 12 further includes an access and outlet assembly 26 supported by the end wall 24. The access and outlet assembly 26 includes a hose 28 which is adapted to receive the hollow discharge area from the container 18, and a mouth discharge outlet 30 in fluid

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concentrations with the hose 23. The waste discharge outlet 20 is advantageously located in the open of the end wall 24 and oriented so that no aerosol phase penetrates along the central longitudinal axis 32 of the canister. The outlet 20 preferably has an internal diameter at the exit of less than about 0.025 inch, and more preferably between about 0.025 inch and about 0.012 inch.

Then, upon the canister 11 being depressed to the downward position in FIG. 1, a measured volume of medication will be discharged from the hose 23 and out the outlet 20 as there is generally critical phase of aerosolized medication within the canister 11, directed generally toward the open end 20 thereof. The inhibitor 10 inhibits forces which promote dispersion and mixing of the aerosolized medication with air within the canister to reduce separation and decrease the velocity of the liquid propellant discharged from the canister 11. More specifically, the inhibitor 10 includes an air tube 34 supported within the canister 11. The air tube 34 has an end 34 which is spaced downstream of and to opposing relationship with the outlet 20.

Discharge outlet 30, and an inlet 31 which is in fluid communication with ambient air outside the canister 11. In the embodiment shown in FIGS. 1-3, the air tube 34 is a bent tube which has a generally axial portion 40 which is generally aligned along the canister's longitudinal axis 32, and a generally radial portion 42 which is oriented in the lower wall 44 of the canister 11. When a user exerts an inspiratory effort on the open end 20 of the canister 11, air is drawn into the canister 11 from the air inlet 31, moving the air into outlet 34 in a direction toward the waste discharge

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Although the embodiment claimed in FIGS. 1-3 and 7 show the air tube 34 bent at an angle of 90 degrees with the portion 40 generally aligned with the axis 41 (FIG. 3) of the waste outlet 30, other arrangements may be used without sacrificing the advantages of the invention. For example, the portion 40 may be arranged at an obtuse angle (i.e., between about 90 degrees and 180 degrees, 130 degrees being defined as exactly opposite to the direction of a plane ending the outlet 30) to the axis 41 of the waste outlet 30, with the portion 40 of air tube 34 being oriented to direct air jet to the outlet 30. Additionally, the portion 42 which attaches to the canister wall need not be radial, but can be selected as an acute or obtuse angle to the canister wall 44.

The invention further includes features which reduce the likelihood of liquid droplets or dry particles impacting and potentially sticking to the lower walls 34 and 44 of the canister 11. More particularly, the inhibitor 10 includes a plurality of auxiliary air tubes 46 through the end wall 34 and circumferentially spaced downstream as to have an offset from the waste outlet 30. A first circumferential ring of auxiliary air tubes 46 are located upstream the junction 48 between the end wall 34 and the lower wall 44 of the canister 11. A second circumferential ring of auxiliary air tubes 47 are located distally between the junction 48 and the waste outlet 30. An inspiratory effort exerted on the open end 20 of the canister 11 causes air to flow into the auxiliary air tubes 46 and 47 as indicated by arrows 50, and upward direction along the lower wall 44 of the canister 11 and

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outlet 30. The portion 40 of air tube 34 is located and oriented within the canister 11 so that air flowing out from the outlet 30 impinges on a plane of aerosol ending the waste outlet 30. Once this air flow from the tube 34 has been established, the carrying force of the canister 11 is assumed to discharge a plane of aerosolized medication from the outlet 30. The impingement of air from air tube 34 on the plane causes the plane to flow down and be dispersed so as to occupy a larger portion of the cross section of the canister 11. The result is enhanced mixing of the aerosol with air, which promotes more complete respiration of liquid propellant by the time the aerosol enters the open end 20 of the canister 11, and a reduction in velocity of the plane exiting the open end 20 as this approaches the velocity of the inspiratory breath. Accordingly, a greater fraction of the measured dose of medication is deposited from the canister 11 into the open end 20 in the form of respirable dry particles of the optimum size of about one to five microns moving at a relatively low velocity that substantially matches the inspiratory breath velocity, as opposed to relatively large liquid droplets moving at a relatively high velocity. Impaction and sticking of medication within the mouth and throat are thereby reduced.

The air tube 34 and canister 11 can be longitudinally located of one piece, with the lateral passage of the air tube 34 extending through the canister 11 in establish fluid communication with air outside the canister 11. Alternatively, the air tube 34 may be formed of a distal tube bent into the appropriate configuration and attached to the canister 11 at the inlet end 31.

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movement back and forth 52, as indicated by arrows 51. This auxiliary air flow forms a buffer or boundary layer air flow along the lower wall 44 and end wall 34 which tends to reduce the impaction and prevent sticking of medication on lower wall 44 and end wall 34.

To the further refinement of this end, the inhibitor 10 also includes a plurality of vortex generators or vanes 54 (see also in FIG. 2) mounted on the lower wall 44 of the canister 11 and extending inwardly downstream. The vanes 54 are located downstream of the auxiliary air tubes 46, with each vane 54 advantageously being located approximately in axial alignment with one of the auxiliary air tubes 46. The vanes 54 are selected as an angle to the axial direction defined by longitudinal axis 32, so that vorticity and swirl are imparted to air flowing over them. Thus, the boundary layer air flow caused by auxiliary air tubes 46 encounters the vanes 54, which imparts vorticity and swirl to the boundary layer air flow. This vorticity and swirl further reduces the likelihood of aerosol droplets or particles impacting and sticking to the lower wall 44.

As shown in FIGS. 1 and 3, the inhibitor 10 includes a separate expiratory tube 56 which connects to the open end 20 of the canister 11. The expiratory tube 56 has a reduced diameter portion 58 adapted to be inserted into the mouth of a user of the canister 11. After completely exhaling, the user inserts the portion 58 into the mouth with the lips closed around the portion 58, and then begins to inhale, which establishes air flow from the air tube 34 and through the auxiliary air tubes 46. Once

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down air flow are constituted and while continuing to rotate, the rear depresses the casing 12 to discharge a current volume of conditioned and propulsive air from the rear discharge outlet 30. The rear section is liable to fill the lungs to such capacity, and then typically holds the breath for a period of time to allow the inverted section to exhale while the lungs of the lungs.

As shown in FIG. 3, the housing 12 is formed in four sections including the frontpiece 30 which is integrally formed. However, for ease of construction, the housing 12 may alternatively be formed in three main flow sections. For example, the housing 12 may be formed in two sections, a first section including the frontpiece 30, and the second 34, and the mouth 14 up to and including the rear 34, and a second section including the portion of mouth 14 below the rear 34 and the frontpiece 30. Alternatively, the housing 12 may be formed in two sections split on a longitudinal plane through the mouth, the two sections being generally mirror images of each other which are joined together along the plane of symmetry. Nevertheless, for illustrative purposes, an embodiment having four sections is shown and described.

A first section 40 includes the frontpiece 30, the rear wall 34 and section and mouth assembly 36, and a generally cylindrical portion 42 which forms a part of the mouth 14 and is connected to the rear wall 34 at the junction 44. The first section 40 subsequently is integrally formed of one piece, although it may alternatively be formed in multiple pieces which are subsequently joined together.

A second section 46 includes a second generally cylindrical portion 46 which lower and rear diameters are equal to those of the first generally cylindrical portion 42, and a rearward-flaring portion 48 which is integrally received within the rearward flange of the first cylindrical portion 42. The portion 46 has an inner wall 70 which is generally conical, converging slightly in the axial direction toward the frontpiece 30. The rear 34 are mounted on the inner wall 70. Second section 46 preferably is integrally formed of one piece, although it may alternatively be formed in multiple pieces which are subsequently joined.

A third section 72 of the housing 12 includes a third generally cylindrical portion 74 whose lower and rear diameters are equal to those of the second generally cylindrical portion 46, and a rearward flaring cylindrical portion 76 which is integrally received within the rearward flange of the second generally cylindrical portion 46. The rear diameter of portion 76 is approximately equal to the inner diameter of portion 46 so as to provide a slight fit between these parts. The inner surface 78 of portion 76 has a diameter which is approximately equal to the rearward diameter of the conical inner wall 70 so the junction between surfaces 70 and 78 does not present any substantial step in the flowpath defined by the mouth 14. The air inlet 34 is mounted on the lower surface of the third section 72 at the junction between the lower surface 78 and the lower surface 80 of third cylindrical portion 74. A hole 82 through the portion 74 opens with the forward passage of air into 34 to provide fluid communication between the hole 82 of air inlet 34 and

mouth air inside the mouth 14. Third section 72 may be integrally formed of one piece, or formed in multiple pieces and subsequently joined.

The fourth section of the housing 12 is the frontpiece 30, which has a generally cylindrical portion 34 which is integrally received within the rearward flange of the third generally cylindrical portion 74 (which also defines the rear wall 34 of the mouth 14). The portion 34 is attached to an inner flange 36, which is then attached to the rearward flange portion 76 which is located near a rear's mouth. The rear diameter of portion 34 is approximately equal to the diameter of inner surface 80 so as to provide a slight fit therewith.

The housing 12 alternatively is formed of a plastic such as polycarbonate, polyester, polypropylene, polyethylene, ABS, polycarbonate, or polycarbonate. The housing 12 may be constructed by any suitable technique such as injection molding or blow molding.

FIG. 3a shows an alternative embodiment of an alternate and mouth assembly 36 in the interior 34, in cross-sectional view on the horizontal plane. Distinct in FIG. 3, the alternate and mouth assembly 36 includes two spaced-apart discharge outlets 32a which are both fluidly connected to the rear 32b and which converge toward each other in the direction of the mouthpiece 30. Thus, depending on the casing 12 as to discharge a current volume of conditioned air from the rear 32b through two spaced planes to be emitted from the pair of outlets 32a. The planes converge and separate on each side upstream of the air inlet 34.

creating the current on spread out, thereby aiding entry of the current with air. Additionally, impingement of the two planes aids in creating another discharge, which enhances separation of propellant. It will be appreciated that the construction of the housing 12 is shown as being designed in the horizontal direction and the outlets 32a are shown as being spaced apart in the horizontal plane. Alternatively, however, the housing 12 may simply be oriented in the vertical direction and the outlets 32a vertically spaced apart and angled toward each other so as to achieve the desired convergence of the two planes.

FIG. 4 depicts an alternative embodiment of an alternate 10a in which the elongated air inlet 34 of the housing 10 is formed by a curved air inlet in the form of a loop 42a which is supported in the mouth 14 by a pair of helical spacers 42b. In FIG. 4, a pair of helical spacers 42b having the helical "a" profile define parts analogous to those having the same reference numerals without the suffix in FIG. 3, while parts identified with identical reference numerals in FIG. 3 and 4 denote identical parts. Thus, the helical 42a is analogous to the helical portion 42 of the air inlet 34, and the helical 42b are analogous to the helical portion 42 of the air inlet 34. The helical 42a includes a curved cavity 42c of a flow diameter, and an outer passage 42d of a second smaller diameter. The outer passage 42d is generally aligned with the mouth 14 and oriented so that air flowing toward the mouth is directed toward the mouth outlet 30. The forward passage of air into the mouth is made air by a pair of helical 42b through the cylindrical portion 34a. In the

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retrofitting of the inhaler 12b shown in FIG. 4, there is no action of the breathing apparatus in the second stroke 4b of FIG. 4. Thus, the valve 34 have been exhausted from the inhaler 12b. However, the secondary air inlet 46 are still present in the inhaler 12b to provide a temporary lower air flow during the lower half of the stroke 4b.

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FIGS. 5 and 6 illustrate yet another embodiment of an inhaler in accordance with the principles of the present invention. FIG. 5 schematically depicts a horizontal cross section analogous to FIG. 1, showing an inhaler 12b in which the current phase is directed away from the user so that the current must reverse

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direction before being inhaled. FIG. 6 schematically depicts a vertical cross section of the inhaler 12b. Again, the parts are denoted by the reference numerals, while analogous parts are denoted by the letter "b" suffix. The inhaler 12b includes a housing 12b defining a chamber 14b which has a first closed end defined by an end wall 50 and a second open end defined by a mouthpiece portion 52b adapted to be

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inserted into a user's mouth. The mouth 14b has a first larger internal cross-sectional area near the majority of its length, tapering to a second smaller internal cross-sectional area at the mouthpiece portion 52b. The housing further includes a receptacle portion 14b which protrudes from the mouth 14b in a location between the end wall 50 and the mouthpiece portion 52b. The receptacle portion 14b includes a

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vertical passageway (not shown). The housing 12b further includes an actuator and needle assembly 28 arranged in the bottom end of receptacle portion 14b

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Thus, the second stroke a portion of the length of stroke 4b when, thereby increasing resistance to flow of the current while the device before exiting the mouthpiece 52b. This leads to more complete compression of liquid propellant. Furthermore, the flow-reversed current due to the velocity of the current exiting the

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mouthpiece will be substantially equal to the velocity of the user's inhaled breath, reducing the pressure of impingement to the mouth and throat.

FIG. 7 depicts yet another embodiment of the invention providing automatic actuation of the canister to discharge a dose of medication in response to, and synchronized with, the user's respiratory effort. An inhaler 12c includes a

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housing 12c having a mouth 14c which has an internal passage to connect for inhalation by the user. The mouth 14c is shown to include the air inlet 34 and the secondary air inlet 46. It may also include the valve 34 of inhaler 12. Alternatively, the mouth 14c may be a simple straight tube with an open end for the user of conventional construction. Thus, with the exception that the mouth 14c must adapt

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to provide fluid communication with a chamber 12c in housing 12c as discussed below, the details of the mouth 14c are not important in an understanding of the broad-spectrum features of the invention.

The housing 12c further includes a receptacle portion 14c which is connected to the chamber 12c. The receptacle portion 14c comprises a generally

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cylindrical shape having a longitudinal axis 52c which is oriented in an oblique angle to the longitudinal axis of the chamber 12c. A canister 12 is mounted within the receptacle

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such that the bottom portion 12c of the canister may be inserted into a bore 22 of the actuator and needle assembly 28. The details of the actuator and needle assembly 28 have already been described in connection with FIG. 1. The needle discharge orifice 30 is oriented so as to direct an aerosol phase toward the end wall 50.

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The inhaler 12c includes an internal mouth 52 which is axially disposed with the chamber 12c. The internal mouth 52 has an open end 54 spaced from and adjacent the end wall 50, and a closed end 56 remote from the end wall 50 and defined by an end wall 34c which supports the actuator and needle assembly 28. The inhaler further includes an air inlet 34c oriented in the end wall 50 and axially

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disposed within the mouth 14c. The air inlet 34c however pass way into the lower mouth 52 toward the needle discharge orifice 30. The lower 12b of air inlet 34c is connected to ambient air through the mouth 14c by a tube 58 through end wall 50. The lower 12b of air inlet 34c is in opposing relation to the orifice 30. Accord-

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ing to the orifice 30 causes the flow of lower mouth 52 and pressure

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across the end wall 50 of lower mouth 14c. Inhalation of air flow through the mouthpiece 52b causes air to enter through hole 58 into air inlet 34c and out the lower 14c toward the pharynx. The pharynx and the air flow into the 34c area, causing the pharynx to close down and expand out while lower mouth 52. Continued inhalation by the user causes the diaphragm to rise through the open end 54 of lower mouth 52, and thus reverse direction to flow through the space between the lower mouth 52 and the lower mouth 14c, and draw through the mouthpiece 52b.

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portion 14c with its longitudinal axis aligned with the longitudinal axis of the receptacle portion 14c. Disposed between the receptacle portion 14c and the chamber 12 is an inner sleeve 120. The inner sleeve 120 has an open top end 122 through which the canister 12 may be inserted, and an open bottom end 124 which is

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arranged such that the canister 12 cannot go through it but which nevertheless permits the bottom end 12 of the canister to be inserted into the bore 22 of actuator and needle assembly 28. More specifically, the sleeve 120 extends between end 124 has inwardly extending flanges 122 which abut the top portion 120 of the canister. The canister 12 is slidable within sleeve 120 along the direction defined by the

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longitudinal axis 120 of receptacle portion 14c so as to permit the canister to be depressed toward the actuator and needle assembly 28 in order to actuate the canister's ejection valve.

The inner sleeve 120 is also slidable within the receptacle portion 14c along the direction of axis 120 for the purpose of placing the canister 12 in a retracted position ready to be actuated. The receptacle portion 14c has two longitudinal slots 110 circumferentially spaced apart about 90 degrees, one of which receive a pair of diametrically opposite lugs or ears 112 extending outwardly from the outer surface of lower sleeve 120. Alternatively, the receptacle portion 14c may have only one slot 110 spaced 180 degrees apart and receiving the lugs 112. Thus, as the inner sleeve 120 slides longitudinally within receptacle portion 14c, the lugs 112 slide longitudinally within the respective slot 110.

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The initiator includes a generally cylindrical can ring 114 which fits over the outside of reciprocating portion 146. The can ring 114 has an annular flange 116 at its lower end which extends outward beyond the outer surface of the housing 10 so as to facilitate gripping of the can ring 114 by the user's hand. The lower portion 118 of ring 114 has a pair of circumferentially extending recesses or can tracks 120 formed therein approximately 120 degrees apart which extend longitudinally upward to the open top end 122 of can ring 114. Each can track 120 presents a generally helical surface 124 to facing relationship with one of the legs 112 protruding outwardly from the lower shroud 122 through slot 118. Thus, mating with the can ring 114 is a piston 126 in which each leg 112 is in contact with the lowermost portion of the respective can track 120. That is, the portion of can track 120 which is thickest from the top end 122 of can ring 114, reaches of the can ring 114 through the slot defined by the can tracks 120 around the legs 112 so that along the helical surfaces 124 and thereby upwardly advance the lower shroud 122 in the longitudinal direction toward the top end 122.

The upward movement of the lower shroud 122 drives the canister 18 upward by virtue of the helices 124. Rotating this upward movement of the canister 18 is a compression spring 128. The spring 128 is attached to the lower surface of a removable end cap 122 which surrounds the top end 122 of the reciprocating portion 146 and the top end 122 of the can ring 114 to completely enclose the canister 18 in the housing. When the end cap 122 is then released, the spring 128 forces upward the end

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of the canister 18, forcing the canister downward toward the actuator and nozzle assembly 24. With nothing to oppose the downward movement of the canister 18, the spring 128 would move the canister downward until the discharge stop 19 were fully depressed from the canister so as to cause discharge of a measured volume of the canister contents. However, the initiator 10 includes a mechanism which engages the canister to prevent this downward movement, with the mechanism being responsive to an imaginary effort of a user exerted on the open end of the canister 18 so as to discharge from the canister during the user's intention to allow the spring 128 to move the canister back to discharge position.

To these ends, the initiator 10 includes a plunger assembly 132 which is mounted relative to the canister 18 along its axis 134 generally centered in the longitudinal axis 106. The plunger assembly 132 includes a chamber shroud 136 having a distal 138 extending generally downwardly toward the actuator and nozzle assembly 24 from both sides of the axis 134. A first portion 140 of the distal 138 protruding from the side of the shroud 136 moves from the canister engages a recess 142 in a wall 144 of the housing, the recess 142 guiding the movement of the plunger assembly 132 along axis 134. A second portion 146 of distal 138 protruding from the side of the shroud 136 facing the canister extends through an opening 148 in reciprocating portion 146, terminating at an enlarged head end 150. A compression spring 152 is captive between the head end 150 and the wall of the reciprocating portion 146, forcing the plunger assembly 132 toward the canister 18.

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A helical trigger 154 is attached to the head end 150. The trigger 154 has two spaced-apart parallel prongs 156 (FIG. 8) which extend along the direction of axis 134 to approximately the longitudinal axis 106 of the reciprocating portion 146. The prongs 156 are spaced apart by a distance D which is slightly greater than the diameter of the canister mouth 158 from which the discharge pass 19 protrudes, so as to allow the trigger 154 to pass through the canister mouth 158. Then, when the plunger assembly 132 is fully extended toward the canister 18, the canister mouth 158 causes lower edge portions 160 of the prongs 156, as indicated by the dotted region in FIG. 8. However, when the plunger assembly 132 is withdrawn along axis 134 away from the canister 18, the canister mouth 158 forces the prongs 156 to the rearward of the canister 18 toward the actuator 24 in parallel. The prongs 156 include portions 172 which slope greatly away from the canister mouth 158 in the direction along axis 134 toward the actuator. The portions 172 induce the action of force required for discharge of the trigger 156 from the canister mouth 158.

Movement of the plunger assembly 132 in the direction away from the canister is responsive to air pressure within a variable-volume chamber 162 within the housing. The chamber 162 is defined by the distal 136, the housing wall 144, and a flexible diaphragm 164 which extends to the distal 136 so the wall 144 is a substantially air-tight means. Advantageously, the diaphragm 164 includes a circular portion 166 which lies opposite the side of distal 136 facing the canister 18, and a distal 168 which depends from the outer edge of the circular portion 166 and extends to the housing

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wall 144. Further advantageously, the housing wall 144 comprises a removable cover 170 of the housing, and its edge of the distal 168 is attached to the housing by being sandwiched between the cover 170 and the remainder of the housing. The circular portion 166 of diaphragm 164 includes a central hole through which the distal 138 extends and which slightly surrounds the distal 138 to provide a substantially airtight seal therebetween.

The removable cover 170 includes a recess 172 facing the distal 136 which aligns with a passage 174 formed in a distal 176 of the housing. The passage 174 extends toward the open end 22 of canister 18. The canister 18 is formed in at least two sections, a first generally cylindrical section 62a which includes the distal 176 and is connected to the end wall 24 through which the nozzle extends 26 outward, and a second generally cylindrical section 74a which includes the side wall 24 and which connects to the first section 62a. The passage 174 terminates at the end of first section 62a which connects to second section 74a. A passage 178 through a distal 180 of the second section 74a is directly connected with and forms an extension of passage 174. The passage 178 extends from the lowermost portion 182 of the side wall 24. A second 184 is located near the top end of passage 182. The passage 184 includes a circular portion or throat 186. Air passages 188 extend through the second wall 24 in the vicinity of the throat 186. The second 184 is disposed in passage 182 such that the air passages 188 align with the passage 178. Thus, fluid communication is provided between the second chamber 180

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and the variable-volume chamber 162 by air passages 172, passage 178 is moved between 74a, passage 174 is then section 62a, and section 172 is cover 176.

It will therefore be appreciated that when a user inhales through the open end 20a of chamber 16a, air is drawn from outside the chamber 16a through air tube 34 into the primary air passage of the chamber 16a. This air flow is from through the vent 134, and consequently a below-atmospheric air pressure exists in the vented down 134. This below-atmospheric air pressure is communicated to the chamber 162, with the result that the walls of the chamber 162 are subjected to a force proportional to the pressure difference between atmospheric pressure outside the chamber 162 and the below-atmospheric pressure inside the chamber 162.

Consequently, air within the chamber 162 begins to overcome the chamber 162 through means 172, through passages 174 and 178, through passages 152, and into the vented down 134, and thence through the air tube 34 into the primary air passage of the chamber 16a.

As the user continues to inhale through the chamber 16a, expansion of air from the chamber 162 causes the volume in chamber 162 to decrease, with the result that the stem 136 and the shaft 132 begin to move upward the wall 144 against the force of the spring 132. Accordingly, the trigger 134 begins to move so as to discharge the pump 136 from the chamber 162. When the decrease in volume is sufficient to move the trigger 134 far enough to totally discharge the pump 136 from the chamber 162, contraction of the chamber 162 toward the volume 20 is no longer

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expelled, and the force of spring 132 moves the chamber 162 toward so as to cause contraction of the chamber's contracting volume. A limited flow of compressed medication is thereby discharged from each of the 30 into the chamber 16a for inhalation by the user.

After the trigger 134 has been actuated to depress a dose of medication, it must be retracted so that it is ready to be discharged again. To this end, the user grasps the ring 114 and moves it with respect to the housing 12; through the act defined by the act 12a 12b. This causes the lower down 130 and chamber 18 to be tilted upward against the force of spring 126. When the chamber 18 is tilted upwardly sufficiently to allow the trigger 134 to clear the chamber 162, the spring 132 urges the trigger 134 toward the chamber 162 so that the trigger 134 once again is in a fully extended position to engage the chamber 162. The user then causes the ring 114 back to its starting position to lower the chamber 18, whereupon the chamber 162 once again the pump 136 of the trigger 134. The trigger 134 is then ready to be used again.

It will be appreciated that the breath-synchronous device described above provides no inhibitor in which discharge of medication is immediately responsive to the user's inspiratory effort, so that the user does not have to carefully coordinate the timing of a chamber with the inhalation. Furthermore, discharge of medication does not occur instantaneously upon the user beginning to inhale on the open end of the device, but rather is somewhat delayed until the volume of chamber 162

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has decreased enough to cause activation. It will thus be appreciated that the degree of flow delay between inhalation of a breath and activation is dependent on a number of factors, the primary factors being the cross-sectional area of the chamber 162 and the spring constant of the spring 132, since a discharge of medication requires a certain minimum travel of the chamber 18 to cause the discharge area 19 to be fully depressed, and the travel is proportional to the pressure difference across the chamber 162 in cross-sectional area divided by the spring constant. Accordingly, the trigger 134 may be designed with appropriate selection of these factors so as to achieve activation of the chamber 18 near the peak of a user's inhalation.

Moreover, the trigger 134 provides breath-responsive movement of the chamber 18 which automatically adjusts to the user's rate of inhalation to discharge the medication near the peak of the inhalation. I.e., near the point at which 50 percent of the volume which the user will eventually breathe with a full inhalation has been inhaled. For instance, if a user with normal lung function inhales quickly enough, the open end 20a, air will be exhausted from the chamber 162 more rapidly so as to achieve activation in a relatively short time. Conversely, if a user with impaired lung function inhales slowly through the open end 20a, air will be exhausted more slowly from chamber 162 so as to achieve activation in a relatively longer time.

The trigger 134 further includes an adjustment screw 190 which extends through the housing 12a into the passage 174 so that a restriction within passage 174. By turning the screw 190 one direction, the screw 190 causes further

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into passage 174 to increase the restriction, and by turning the screw 190 the opposite direction, a restriction to decrease the restriction. Thus, the timing of activation of the chamber 18 is adjustable in a particular patient's inhalation may be varied by adjusting the screw 190. Varying the screw position results in a variation in pressure difference across the walls of the variable-volume chamber 162 as a given flow rate

into the open end 20a of chamber 16a. Thus, for a given flow rate into the open end 20a of chamber 16a, turning the screw 190 to increase the restriction of passage 174 will increase the flow period required to overcome the chamber 162 sufficiently to cause activation, whereas turning the screw 190 to decrease the restriction will decrease such flow period.

FIG. 9 depicts a substantially of yet another embodiment of an inhibitor having features for accurate breath activation of discharge. In this embodiment, the trigger 134 is actuated and the discharge pump assembly 132 is exposed by a resiliently compressible bellows 200 which is disposed between a front wall 202 of the housing (not shown) and the chamber 162. The bellows 200 itself acts as the member which keeps the chamber 162 in a non-extended position, the bellows being compressed by air pressure into a position, permitting the chamber 162 to move into a discharge position.

The bellows 200 is subsequently made of elastic material and has a front wall 204 at the end adjacent the chamber 162, the front wall 204 being integrally formed with the activation-defined area wall 206. The bellows 200 has a

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central end wall 228 at the end adjacent the bearing wall 225, the end wall 228 also being integrally formed with the side wall 226. The second end wall 229 is placed by a side or end wall 230 which constitutes an air passage from the interior of the bellows 220. The member 229 subsequently is a member and also similar to a symmetrical member and is integrally formed as one unit with the end wall 228 by casting or other suitable techniques. The end wall 229 of the member 229 consists in a member 231 to the front 234 of a vertical 235. The member 231 is disposed within a side 232 which extends from an end wall 220 which draws air from outside the intake housing, in an end wall 222 which is arranged within the central 10 end thereof opposite the main discharge outlet 20. The side 231 and member 234 may also be formed of suitable metal.

A superimposed plate 236 is attached to the lateral end wall 204 of the bellows 220. The superimposed plate 236 causes the member 231 to 15 throughout the range of motion undergone by the bellows 220 during a rest or ready position to a discharge position. The bellows 220, via the superimposed plate 236, causes a spring force on the member 231. The force of the bellows 220 acts in a direction tending to move the member 231 away from the 20 member 23. Additionally, as is well known, the member 231 carries an internal spring (not shown) which acts between the member body and the bellows end wall 19 in a direction tending to move the member 23 away from the member 23. The spring constant of the bellows 220 is selected such that the force of the spring force

causes, air pressure is again regulated inside and outside the bellows 220, and the bellows 220 returns to its starting position. The force of the bellows 220 and internal spring forcing the member 23 back against the force of the spring 236 into the ready position. Thus, with the device-structure system depicted in FIG. 3, there is no need for a separate cooling system.

The bellows 220 preferably has a spring constant of about 1 pound per inch to about 15 pounds per inch, and a cross-sectional area of about 0.2 to about 0.75 square inch. Thus, a pressure differential of about one pound per square inch across the bellows 220 is sufficient to compress the bellows 220 by an amount of 10 about 0.025 inch to about 0.100 inch. With a constant surface 15, only about 0.025 inch of relative movement is required between the discharge inlet 19 and the member body in order to cause discharge. Accordingly, the member 234 does not need to move a large distance within the device 234 of about one pound per square inch.

While the present invention has been described by a description of various embodiments and while these embodiments have been described in considerable detail, it is not the intention of the applicant to restrict or to limit any 15 form or scope of the appended claims to such detail. Additional embodiments and modifications will readily appear to those skilled in the art. For example, while the bellows which are described and described have the member 231 in communication with intake air via a passage through the member wall, the member 231 may alternatively draw air through one of the auxiliary air lines 45 to the end wall 24, or

caused by the bellows 220 and the force caused by the internal spring is slightly greater than the force caused by the spring 236 (FIG. 7) which causes a force on the end of the member 23 in the direction to tend to move the member 23 toward the member 23 into a discharge position. Thus, at 234, with atmospheric pressure acting both inside and outside the bellows 220, the bellows 220 and internal spring overcome the force of the spring 236 and thereby keep the member 23 in a ready position preventing discharge of conditioned discharge.

However, when a new intake through the intake (not shown) of the intake, air is drawn through the side 231, as previously described in connection with the bellows 220, which causes a low pressure within the device 234 of member 234. This low pressure is communicated via the member 231 and member 232 to the interior of the bellows 220. As a result, the pressure within the bellows 220 is less than the atmospheric pressure which surrounds the outside of the bellows 220, and therefore there is an air pressure force caused on the lateral end wall 204 in the 10 direction toward the bearing wall 202. The sum of this air pressure force and the force of the spring 236 exceeds the spring force caused by the bellows 220 and the member 23 toward the bearing wall 202. By virtue of the force caused on the member 23 by the spring 236, the member 23 is moved away from the end wall 204. With continued 20 evacuation of air from the bellows 220, the member 23 is moved away by discharge position. Once the user completes his intake and air flow through the member 234

through any arrangement having the member 234 outside the primary air passage defined by the intake member. Additionally, the member 234 of FIG. 3 may alternatively be used in the intake configuration depicted in FIG. 7, with the bellows 220 replacing the plate assembly 132 and the lateral end wall 204 of the bellows 220 being attached to the lateral member 134, and the spring 132 being 5 clamped by virtue of the auxiliary of the bellows 220. The invention in its broader aspects is therefore not limited to the specific details, representative apparatus and methods, and illustrative examples shown and described. Accordingly, apparatus may be made from such details without departing from the spirit or scope of applicant's general inventive concept.

With reference to the use of the word "comprising" or "comprising" or "including" in the foregoing description, these words are used in the broad and clear understanding that they are to be interpreted inclusively, rather than 15 exclusively, and the use of these words is to be as interpreted in construing the foregoing description under the following claims.

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The claims defining the invention are as follows:

1. An aerosol flow control apparatus providing automatic discharge of medicament responsive to an inspiratory effort of a user, the apparatus comprising:
a pressurized container of medicament including a container body and a hallow discharge arm which is movable with respect to the container body between an inoperative position in which discharge of medicament is prevented and an operative position in which medicament is discharged through the discharge arm;
a housing adapted to support the container and permit movement thereof between a first position in which the discharge arm is in the inoperative position in a second position in which the discharge arm is in the operative position, the housing further defining a primary air passage including an inlet through which a user can inhale and also defining a secondary air passage extending between the primary air passage and ambient air outside the primary air passage, the secondary air passage including a vented hallow a float;
a variable-volume device supported within the housing and including a wall which is movable with respect to the housing, the variable-volume device defining a variable-volume chamber (herein to be called communication) with the vented float;
a container neck affixed to the movable wall of the variable-volume device, the container neck being movable with the movable wall from a rest position in which the container is in the first position and relative movement between the container body and discharge arm is prevented, to a discharge position in which the container is free to move into the second position;
a resilient member which urges the container into the second position upon movement of the container neck into its discharge position; and
the variable-volume chamber being in fluid communication with the primary air passage, whereby inhalation of a user through the outlet causes air to be drawn through the vented float thereby causing a low pressure in the float which is communicated in the variable-volume chamber, the low pressure causing air to be evacuated from the chamber and thereby cause the movable wall to move the container neck into the discharge position.
2. The aerosol flow control apparatus of claim 1, wherein the vented float is connected to the chamber by a third air passage within the housing, and further comprising an adjustment device which may be selectively positioned to selectively vary the flow rate

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4. The aerosol flow control apparatus of claim 1, wherein the variable-volume device comprises a resiliently compressible bellows, the bellows being disposed between a neck of the container and a wall of the housing which faces the container neck, the movable wall being on one wall of the bellows, the container neck being affixed to the end wall and contacting the container neck, the bellows being compressible toward the housing wall in a direction substantially parallel to the direction in which the container neck moves from the first position to the second position, the bellows being adapted to exert a spring force on the container neck to urge the container toward the first position, the spring force exceeding the force exerted on the container by the resilient member by a predetermined amount which is selected such that when a user inhales through the outlet of the housing, the pressure force caused on the end wall of the bellows by the difference between atmospheric pressure outside the bellows and the low pressure inside the bellows exceeds the predetermined amount, thereby causing the end wall to compress the bellows toward the housing wall and move the container neck into the discharge position such that the container is moved into the second position by the resilient member.

7. A method for delivering a dose of medicament using an aerosol delivery apparatus which houses a medicament-containing container having a container body and a hallow discharge arm movable with respect to the container body between an inoperative position in which discharge of medicament is prevented and an operative position in which medicament is discharged through the discharge arm, with the container being movable within the apparatus between a first position in which the discharge arm is in the inoperative position and a second position in which the discharge arm is in the operative position, the apparatus including a housing defining a primary air passage having an inlet through which a user can inhale and a secondary air passage, the apparatus defining a discharge of medicament from the container with an inspiratory effort of a user through the outlet, the method comprising:
placing the container in the first position;
preventing movement of the container into the second position by a container neck which engages the container to prevent said movement and which is movable in response to below-atmospheric air pressure within a variable-volume device arranged within the housing, the variable-volume device defining an air discharge device, the container neck being movable to permit the container to move into the second position upon a predetermined decrease in pressure of the air chamber;
urging the container toward the second position;

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through the third air passage at a given flow rate through the primary air passage, thereby varying the timing of medicament discharge in relation to the inhalation cycle of a user.

3. The aerosol flow control apparatus of claim 1, wherein the variable-volume device comprises a piston which is axially mounted to a wall of the housing by a flexible diaphragm, and the container neck includes a member which is attached to the piston and which is the most proximal member into the path traveled by the container between the first and second positions so as to prevent the container from moving into the second position, evacuation of air from within the chamber of the variable-volume device causing the piston to move toward the housing wall and thereby withdraw the member from the discharge position permitting the container to move into the second position.
4. The aerosol flow control apparatus of claim 1, wherein the housing comprises a main body portion which receives the container, and an end cap which covers the end of the container opening from the end with the discharge arm and which engages the main body portion to prevent inadvertent removal therefrom, the resilient member comprising a compression spring between an inner surface of the end cap and the container neck that the spring bears against the container when the end cap is engaged with the main body portion.
5. The aerosol flow control apparatus of claim 1, wherein the main body portion includes a generally cylindrical receptacle having a longitudinal axis and defining a generally cylindrical neck in which the container resides, and further comprising a necking device including:
an inner sleeve which encloses the container within the receptacle, the inner sleeve and container being slidable together as a unit within the receptacle along the longitudinal axis, the inner sleeve further including at least one pin extending outwardly from an outer surface thereof through a slot in the receptacle; and
a necking ring which surrounds the receptacle and has a surface which engages the at least one pin, the necking ring being movable with respect to the receptacle so as to move the pin in the direction defined by the longitudinal axis toward the end cap so as to draw the inner sleeve and container upward and thereby move the container into a closed position which permits the container neck to move into its rest position, thereby restoring the apparatus for automatic response to the inspiratory effort of a user.

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upon a user inhaling through the outlet, drawing air through a secondary air passage arranged within the housing, the secondary air passage extending from the primary air passage to ambient air outside the primary air passage, the secondary air passage including a vented hallow a float; and

at least during the drawing step, providing fluid communication between the first position of the vented float of the secondary air passage and the variable-volume chamber so as to communicate a below-atmospheric air pressure caused by the vented float to the air chamber and thereby cause the chamber volume to decrease, whereby the container neck moves to permit movement of the container into the second position to discharge medicament when the predetermined decrease in chamber volume is reached.

6. The method of claim 7 wherein the third position of the vented float is a retracted transverse flow open relative to the neck of the secondary air passage such that the air pressure in the third position is lower than the air pressure in the neck of the secondary air passage when air is flowing therethrough.

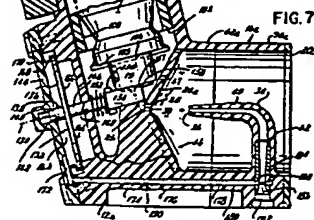
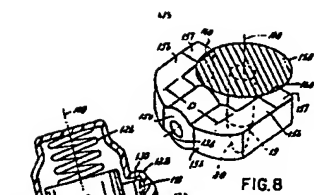
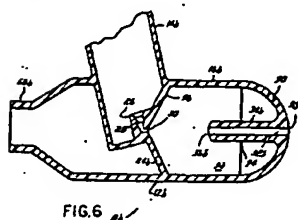
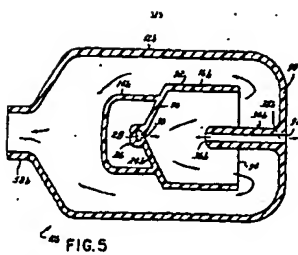
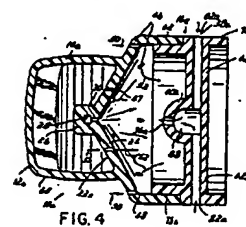
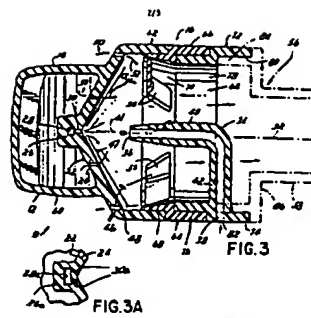
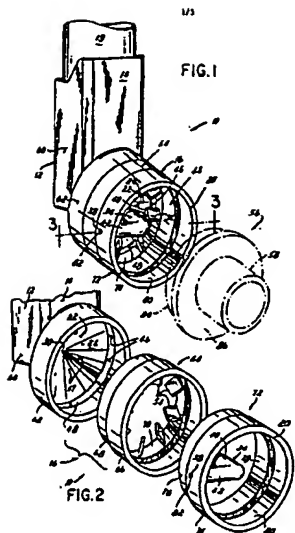
DATED this 14 day of July 1984

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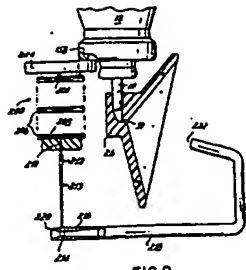


FIG. 9